ENVIRONMENTAL ASSESSMENT

APPENDIX G

Traffic Noise Analysis



Traffic Noise Analysis

Bryant Pkwy. Extension (S) – ARDOT No. 061705 Highway 183 to Shobe Road Bryant, Saline County, AR





Prepared For:

City of Bryant

July 2020





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1.0 Executive Summary

This traffic noise analysis was conducted as a result of partial funding and approvals provided by the Arkansas Department of Transportation (ARDOT) and Federal Highway Administration (FHWA) and included as an attachment to an Environmental Assessment (EA) for Alternative 2 of Bryant Parkway, located in Bryant, Saline County, Arkansas. Refer to the Site Location Map in **Appendix A**.

The analysis included FHWA Traffic Noise Model (TNM) 2.5 model validation, ambient field measurements, and noise predictions based on future growth patterns for Alternative B. Detailed analysis of Alternatives B and D are included in the EA. The noise sensitive land uses for this project are considered to be residential dwellings located in Cherry Creek and Hidden Forest subdivisions and Alcoa 40 Park. Four ambient noise measurements were collected between existing Highway (Hwy.) 183 and Shobe Road at representative locations adjacent to these subdivisions to document the ambient noise levels and for model validation purposes. Predicted noise levels were determined and compared to the FHWA Noise Abatement Criteria (NAC) and ARDOT's Policy on Highway Traffic Noise Abatement for determination of impacts.

A noise screening was conducted for EA Alternatives B and D, which indicated no impacts within the 63 decibel (dB) threshold for NAC Activity Categories B and C. However, substantial increase impacts, as defined by ARDOT, had reasonable potential to occur. As a result, a detailed traffic noise analysis was performed. For screening analysis purposes, the ARDOT noise policy requires determining noise levels within 4 dBA of the NAC value. The screening analysis threshold would therefore be 63 dBA for Activity Categories B and C.

Under current conditions, no residential dwellings are impacted (66 dB(A) Leq(h) or greater). Additionally, based on the proposed project and the 2040 design year traffic volumes, no residential dwellings or park facilities will approach, meet, or exceed the 67 dB(A) Leq(h) for NAC Categories B and C or experience substantial increase impacts.

2.0 Project Description

This proposed roadway would improve the north/south flow of traffic and emergency vehicle response time between the south side of Bryant and the northeast side of Bryant by providing an alternate route to the heavily congested Hwy. 183 (also designated as Reynolds Road). The project would also provide enhanced connectivity and development potential for the Saline County Regional Airport (SUZ).

Alternative B is 2.57 miles in length and begins 0.37 mile east of the intersection of Hwy. 183 and Hill Farm Road. The alignment extends to the south end of Mustang Trail, then continues north of Mustang Trail on new alignment along the western boundary of SUZ to Shobe Road. In order to provide enhanced access to SUZ, a new airport entrance road is proposed between Bryant Pkwy, and the airport terminal building. Alternative B includes portions of a bike/pedestrian trail,





avoids SUZ Runway Protection Zones (RPZ), and crosses the Union Pacific Railroad (UPRR) and Crooked Creek before tying into Shobe Road in the same manner as Alternative D. Construction is planned to begin in the fall of 2020 and be completed in the spring of 2022.

3.0 Fundamentals of Noise and Sound Theory

Noise, defined as unwanted or excessive sound, is an undesirable by-product of our modern way of life. From these known effects of noise, criteria have been established to help protect the public health and safety and prevent disruption of certain human activities. These criteria are based on such known impacts of noise on people as speech interference, sleep interference, physiological responses, hearing loss and annoyance. Highway traffic noise is a major contributor to overall transportation noise and is considered to be a line source of energy from which the energy levels dissipate vertically and laterally from the roadway. Traffic noise is not constant; it varies as each vehicle passes a point. The time-varying characteristics of environmental noise are analyzed statistically to determine the duration and intensity of noise exposure. In an urban environment, noise is made up of two distinct parts. One is ambient or background noise. Wind noise and distant traffic noise make up the acoustical environment surrounding the project. These sounds are not readily recognized but combine to produce a nonirritating ambient sound level. This background sound level varies throughout the day, being lowest at night and highest during the day. The other component of urban noise is that it can be intermittent and louder than background noises due to a number of sources such as manufacturing, railroads, and local airports. It is for these reasons that environmental noise is analyzed statistically.

Sound from highway traffic is generated primarily from a vehicle's tires, engine and exhaust. Sound intensity decreases in proportion with the square of the distance from the source. Generally, sound levels for a point source will decrease by 6 dB(A) for each doubling of distance. Sound levels for a highway line source vary differently with distance because sound pressure waves propagate along the line and overlap at the point of measurement. Sound is commonly measured in decibels (dB) which are logarithmic units and are not added arithmetically as opposed to the more common linear units such as temperature. Sound pressure level from two equal sources is 3 dB greater than the sound pressure level of just one source. So, two trucks producing 90 dB each combine to produce 93 dB, not 180 dB. In other words, a doubling of the noise source produces only a 3 dB increase in the sound pressure level. Studies have shown that this increase is barely perceptible by the human ear. Sound occurs over a wide range of frequencies. However, not all frequencies are detectable by the human ear; therefore, an adjustment is made to the high and low frequencies to approximate the way an average person hears traffic sounds. This adjustment is called A-weighting and is expressed as dBA. In addition, because traffic sound levels are never constant due to the changing number, type and speed of vehicles, this noise analysis will discuss noise levels as Leq(h). Leq is defined as the steady-state sound level which, in a stated period of time, contains the same acoustic energy as the timevarying sound level during the same period. Leq(h) is the hourly value of Leq and is based on the dBA unit.





4.0 Methodology and Criteria for Determining Impacts

Traffic noise analysis consists of a comparison of physically measured or modeled noise levels for the existing condition with projected noise levels for the future condition. The analysis was performed using TNM 2.5 to model existing and future noise levels based on traffic data, roadway geometry, and receiver site locations. A receiver is a location, usually representing a dwelling unit, where frequent exterior human activity occurs. The chosen receiver is modeled for noise levels and evaluated for noise impacts. The noise analysis conducted for this project was consistent with FHWA and ARDOT policy and 23 CFR Part 772. Methodology included identification of sensitive noise receptors, recording ambient noise levels at four (4) locations along the proposed project, and predicting no-action, existing, and design year build noise levels. Traffic data was recorded during one set of noise measurements to validate the TNM model.

The FHWA has seven noise activity categories based on land use and sound levels, each of which has its own Noise Abatement Criteria (NAC). The NAC categories are listed in **Table 1**. If a project would result in higher Leq(h) values than the NAC values for a given location, then noise abatement or mitigation measures must be evaluated.

		ble 1: FHWA Noise Abatement Criteria (NAC) dourly A-Weighted Sound Level, decibels dB(A)
Activity Category	Activity Criteria ¹ Leq(h) ²	Activity Description
А	57 (Exterior)	Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose.
B ³	67 (Exterior)	Residential
C ₃	67 (Exterior)	Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, day care centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreational areas, Section 4(f) sites, schools, television studios, trails, and trail crossings.
D	52 (Interior)	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public or nonprofit institutional structures, radio studios, recording studios, schools, and television studios





		ble 1: FHWA Noise Abatement Criteria (NAC) dourly A-Weighted Sound Level, decibels dB(A)
Activity Category	Activity Criteria ¹ Leq(h) ²	Activity Description
E ³	72 (Exterior)	Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in A-D or F.
F		Agriculture, airports, bus yards, emergency services, industrial, logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing
G		Undeveloped lands that are not permitted

¹ The Leq(h) Activity Criteria values are for impact determination only, and are not design standards for noise abatement measures.

5.0 Noise-Sensitive Land Uses

The project area is surrounded by residential, airport, park and undeveloped properties. There are two adjacent residential subdivisions (Cherry Creek and Hidden Forest), which were evaluated as NAC Activity Category B receptors and Alcoa 40 Park, which was evaluated as a NAC Activity Category C receptor. The airport property would be considered a NAC Activity Category F property. No other sensitive receptors associated with NAC activity categories A, D, and E were evaluated.

Twenty-one (21) receptor locations representing thirty-two (32) receptors were selected for modeling purposes to identify noise levels for the no-action, existing and design year conditions. Receptor locations are shown in **Figure 1**.

6.0 Determination of Existing Sound Levels

Garver conducted noise measurement readings on June 2, June 22, and July 21, 2020 in the PM peak traffic hours of 4pm to 7pm for use in the noise model validation and documenting ambient noise conditions.



² The equivalent steady-state sound level which in a stated period of time contains the same acoustic energy as the time-varying sound level during the same time period, with Leq(h) being the hourly value of Leq.

³ Includes undeveloped lands permitted for this activity category.



6.1 Validation

Existing noise measurements were recorded at one model validation (MV) location adjacent to the study area along Shobe Road for validation purposes. This location was chosen as a result of being the only major connecting roadway within the project limits with appreciable traffic to correlate to TNM predictions. A total of four measurements were collected at in the same location. Refer to **Figure 1** for measurement and receptor locations and **Table 2** for model validation results. TNM-predicted noise levels differed from actual measured levels by -2.2 to -2.3 dB(A) for two of the four measurements at the validation location, which is within the required 3dBA validation criteria. Therefore, the TNM model was validated. A Larson Davis LxT Model 831 noise meter was utilized to record model validation measurements for a duration of 15 minutes each.

	Table 2: Vali	dation Measurements	
		odel Noise Levels Comparis ternative B	on
Receptor	Field Record Noise Level dB(A) Leq(h)	TNM Predicted Noise Level dB(A) Leq(h)	Difference (Model-Field)
MV-1a	64.5	61.1	-3.4
MV-1b	63.2	61.0	-2.2
MV-1c	63.7	59.8	-3.9
MV-1d	63.5	61.2	-2.3

6.2 Ambient Measurements

Due to the entire project being on new alignment, ambient noise level measurements were collected for 20 minutes at four locations in close proximity to adjacent residential subdivisions, as shown in **Figure 1**. Trains, airplanes, weather conditions, resident interaction, and other noise sources were also documented during the recording sessions. SUZ and the UPRR, which crosses the proposed alignment, also contribute to the existing noise environment. Ambient measurement results are contained in **Table 4** with overall modeling results.

6.3 Traffic Data

Traffic volumes were analyzed using traffic data from the ARDOT and travel demand outputs from the Central Arkansas Regional Transportation Study (CARTS) developed by Metroplan (Garver Feasibility Study, 2017). The existing year of 2020 and future design year was determined to be 2040. The unit of measure for roadway traffic is the average annual daily traffic (AADT), which is defined as the estimate of traffic volumes in vehicles per day on a roadway, averaged from the





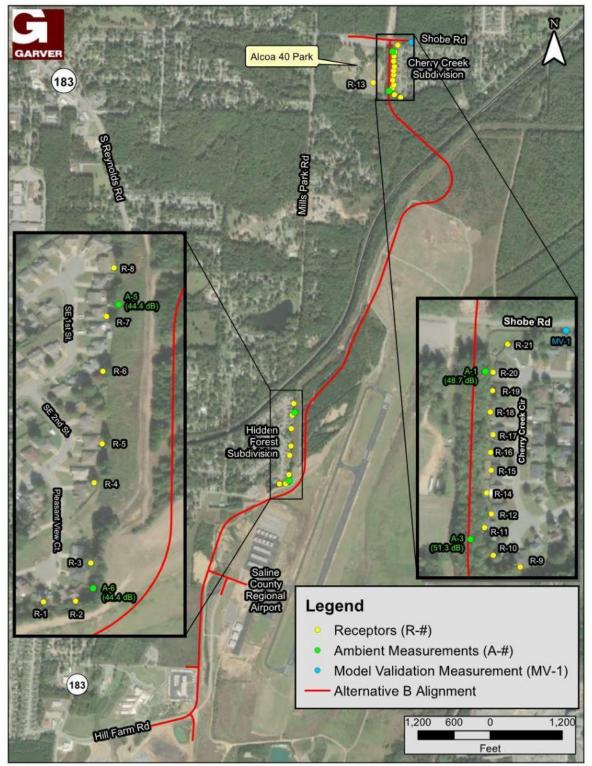


Figure 1 - Noise Measurement and Receptor Locations



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seven annual average days of the week, for a calendar year. TNM utilizes the design hourly volume (DHV) to determine the existing traffic noise levels and calculates the predicted noise levels that occur when the highest volume for an hour is combined with the highest speeds and considered as the "worst hour for noise." DHV data is based on the percentage of hourly vehicular traffic present on the facility at the design capacity consisting of cars, medium trucks, and heavy trucks. **Table 3** depicts the DHV values utilized in the modeling. TNM modeling assume vehicles were traveling 30 mph on Shobe Road during both existing and future conditions. Existing traffic conditions in the area are predominantly car traffic with very few medium and heavy trucks. The proposed speed limit is 35 mph for Alternative B and therefore the modeling assumed all vehicles were traveling at 35 mph for design year conditions.

	Table	3: Noise M	odel Traffic	Volumes	
Year	AADT	DHV	Cars	Medium Trucks	Heavy Trucks
	Shob	e Road Wes	t of Bryant F	Parkway	
Existing (2020)	4,585	504	489	11	5
Future (2040)	5,135	565	548	12	5
	Shob	e Road East	of Bryant P	arkway	
Existing (2020)	3,310	364	353	8	3
Future (2040)	4,063	447	434	9	4
		Alterr	native B		
Existing (2020)	-				
Future (2040	4,622	508	493	11	5
	Bryar	nt Parkway N	orth of Shol	be Road	
Existing (2020)	5,120	563	546	12	5
Future (2040)	7,750	853	827	18	8
No	-Action Alterna	ative – Bryan	t Parkway N	lorth of Shobe Road	d
Existing (2020)	5,120	563	546	12	5
Future (2040)	5,144	566	549	12	5
Ne	o-Action Alterna	ative – Shob	e Road Wes	t of Bryant Parkway	
Existing (2020)	4,701	517	501	11	5
Future (2040)	5,267	580	563	12	5
N	o-Action Altern	ative – Shob	e Road East	t of Bryant Parkway	
Existing (2020)	3,706	408	396	9	4
Future (2040)	4,549	500	485	11	5



7.0 Determination of Future Sound Levels

The 2040 design year traffic was utilized to determine if future noise levels would exceed the NAC activity category thresholds. Traffic directional splits reviewed for the project indicated that 70% of the traffic would occur in the PM heading northbound and 30% in the AM heading southbound. This directional split was utilized in TNM modeling. This traffic split was utilized to analyze impacts to the Cherry Creek subdivision, which places the higher traffic volumes closer to the subdivision. The opposite peak traffic flow (70% AM southbound and 30% PM northbound) was utilized in analyzing potential impacts to the Hidden Forest subdivision near the south end of the project. **Table 3** identifies the future traffic data utilized and **Appendix B** contains the traffic worksheets showing the directional split traffic data.

The results of the future 2040 Alternative B indicated that none of the residences or facilities within Alcoa 40 park will approach, meet or exceed the 67 dB(A) Leq(h) for NAC Activity Categories B and C. Additionally, there are no substantial increase impacts (i.e., an increase of 10 dBA or more) associated with Alternative B. No future no-action alternative impacts are anticipated. **Appendix C** contains TNM results and layouts and **Appendix D** contains alternative comparisons.

Under Alternative B, twenty receivers may experience minor increases in noise levels (i.e., 0-5 dB increase) and twelve receivers may experience moderate traffic noise increases (i.e., 6-9 dB increase) over existing noise levels.

The no-action alternative will allow for the continued ambient noise levels to remain unchanged and coincide with the increase in traffic on surrounding roadways and development in the area.

	Та	able 4: I	Future Traffic Noise F Alternative		A) Leq (h)		
Receptor*	Dwelling Units	Туре	Distance/Location from Roadway Centerline	Existing 2020 Noise Levels**	Future 2040 Noise Levels	Change (+/-)	Noise Impact?
R-1	2	SFR	135+80, 188' west	44.4	50.0	5.6	N
R-2	1	SFR	137+19' 146 west	44.4	52.1	7.7	N
R-3	2	SFR	139+65, 221' west	44.4	47.4	3.0	N
R-4	2	SFR	143+94, 257' west	44.4	47.0	2.6	N
R-5	3	SFR	145+49, 234' west	44.4	48.2	3.8	N
R-6	3	SFR	148+40, 233' west	44.4	48.9	4.5	N
R-7	3	SFR	150+43, 227' west	44.4	48.8	4.4	N
R-8	3	SFR	151+77, 244' west	44.4	47.1	2.7	N
R-9	1	SFR	216+25, 203' east	51.5	50.7	-0.8	N
R-10	1	SFR	217+40, 97' east	51.6	57.1	5.5	N





	Ta	able 4: F	Future Traffic Noise F	•	(A) Leq (h)		
			Alternative	В			
R-11	1	SFR	218+50, 60' east	51.7	60.3	8.6	N
R-12	1	SFR	219+07, 87' east	51.7	58.3	6.6	N
R-13	1	Р	219+45, 254' west	51.9	50.1	-1.8	N
R-14	1	SFR	219+93, 72' east	51.8	60.0	8.2	N
R-15	1	SFR	220+75, 79' east	51.9	59.0	7.1	N
R-16	1	SFR	221+46, 76' east	52.1	59.2	7.1	N
R-17	1	SFR	222+18, 85' east	50.4	58.3	7.9	N
R-18	1	SFR	223+04, 71' east	51.2	58.4	7.2	N
R-19	1	SFR	223+89, 78' east	52.3	57.6	5.3	N
R-20	1	SFR	224+61, 76' east	54.2	58.9	4.7	N
R-21	1	SFR	225+70, 129' east	55.0	58.5	3.5	N

^{*} Ambient measurements were utilized to account for background noise levels and were applied as follows:

8.0 Consideration of Abatement

Noise abatement would be investigated upon future predicted impacts of receptors receiving noise levels at or above 66 dBA or if noise levels increased 10 dBA or more. The highest noise receptor reading was predicted to be 60.3 dBA in 2040 and the highest predicted increase in traffic noise levels was predicted to be 8.6 dBA for the future design year as shown in **Table 4**. As a result, noise mitigation measures are not considered for Alternative B.

9.0 Construction Noise

Construction noise sources may include heavy machinery such as dozers, trackhoes, scrapers, cranes and large material transport trucks. Noise generated by construction are temporary and often can be minimized by implementing time of day restrictions limited to daylight hours. Temporary noise increases at the Alcoa 40 Park are anticipated; however, construction scheduling and other measures will be considered to minimize potential impacts to users of the park.

10.0 Coordination with Local Officials

Noise levels approaching and/or exceeding the 66 dBA were identified to fall within the proposed right-of-way along the entire project. Therefore, no future land use impacts are anticipated as a result of the project. Public comments that may arise due to the noise study should be coordinated with local officials.



R-1 through R-8 used 44.4 dB; R-9 through R-16 used 51.3 dB; R-17 through R-18 used 48.7.

^{**} Four ambient measurements were collected for a duration of 20 minutes each.

Type: SFR-Single family residential. P-Park

APPENDICES





APPENDIX A

Site Location Map





APPENDIX B

Traffic Data Worksheets



HT30%

W110%

345 148

2040 70%

NOISE DATA WORKSHEET

Job Name: Bryant Parkway - Hwy. 183 to Shobe Rd.

061705

Roadway Reference: B	Bryant Parkway - Proposed	pesod									
County: Saline				ī							
Jesign Year:	2040										
ear(s) To Be Modeled:	2020 2040										
				V-Coordinates	nafec						
loadway Cross-Sections:	2020					_	Note:	DHV = (ADT)(K))(K)		
						_		DDHV = (4	DDHV = (ADT)(K)(D)		
	2040	Proposed						11%	/ - V - V		
						_		K - Percent	K - Percent of ADT occuring in design hour	uring in d	esign hour
Derating Speed:		35						D - Directio	D - Directional Distribution	ion	1
raffic Data:		YEAR	ADT	%TRUCK	DHV	CARS	TM	보	CARS/2	MT/2	HT/2
							%02	30%			
		2020	3,210	3%	353	342	7	3	171	4	2
		2040	4,622	3%	208	493	11	2	246	2	2
	_										
									INL	TNM 2.5 VALUES	LUES
								_	Northbound & Southbound	& Southbo	pund

HT30% 4 2

2020 70% 30%

NOISE DATA WORKSHEET

Job Name: Bryant Parkway Bryant Parkway Bryant Parkway Bryant Parkway Project 1 North of Shobe Rd. Accordinates Roadway Reference: Bryant Parkway Project 1 North of Shobe Rd. Accordinates Accordinates Accordinates Note: DHV = (ADT)(K) DHV = (ADT)(K) DHV = (ADT)(K) ACCORDINATION = (ADT)(K) Accordination design hour procuring in design hou	Operating Speed: 35 35 D - Directional Distribution	Traffic Data: YEAR ADT %TRUCK DHV CARS MT HT CARS/2 MT/2 HT/2	-	7,750 3% 853 827 18		TNM 2.5 VALUES	PROPOSED	2040 CARS MT70% HT30%		30% 248 5 2
---	---	---	---	---------------------	--	----------------	----------	-----------------------------	--	-------------

4 2

NOISE DATA WORKSHEET

Job Name: Bryant Parkway - Hwy 183 to Shobe Rd	to Shobe Rd									
Roadway Reference: Shobe Rd. East (Existing)	ast (Existing)									
County: Saline										
Design Year: 2040										
Year(s) To Be Modeled: 2020	2040									
			Y-Coordinates	nates						
Roadway Cross-Sections:	2020 Existing					Note:	DHV = (ADT)(K)	DT)(K)		
	•		•		_) = \NHQQ	DDHV = (ADT)(K)(D)		
	2040						11%			
							K - Percen	t of ADT oc	curing in	K - Percent of ADT occuring in design hour
Operating Speed:		30					D - Direction	D - Directional Distribution	ution	
Traffic Data:	YEAR	ADT	%TRUCK	DHV	CARS	Ψ	Ħ	CARS/2	MT/2	HT/2
						%02	30%			
	2020	3,310	%8	364	353	8	3	177	4	2

061705

Job Name: Bryant Parkway - Hwy. 183 to Shobe Rd.	wy. 183 to Shobe I	Rd.										
Roadway Reference: Shobe	Shobe Rd. East (Future)											
County: Saline												
Design Year: 2040	40											
Year(s) To Be Modeled: 2020	20 2040											
				Y-Coordinates	nates							
Roadway Cross-Sections:	2020					_	Note:	DHV = (ADT)(K)	OT)(K)			
) = \AHQQ	DDHV = (ADT)(K)(D)			
	2040 P	Proposed						11%				
								K - Percen	t of ADT oc	curing in	K - Percent of ADT occuring in design hour	
Operating Speed:		30						D - Direction	D - Directional Distribution	ıtion	,	
Traffic Data:		YEAR	ADT	%TRUCK	DHV	CARS	Ψ	보	CARS/2	MT/2	HT/2	
							%02	30%				
		2020	3,310	3%	364	353	∞	3	177	4	2	
		2040	4.063	3%	447	434	<u></u>	4	217	2	2	

061705

Job Name: Bryant Parkway - Hwy. 183 to Shobe Rd.	. 183 to Shol	be Rd.									
Roadway Reference: Shobe F	Shobe Rd. West (Existing)	isting)									
County: Saline											
Design Year: 2040											
Year(s) To Be Modeled: 2020	2040										
				Y-Coordinates	nates						
Roadway Cross-Sections:	2020	Existing					Note:	DHV = (ADT)(K))(K)		
) = \HQQ	DDHV = (ADT)(K)(D)		
	2040							11%			
								K - Percen	K - Percent of ADT occuring in design hour	curing in c	lesign hour
Operating Speed:			30					D - Directio	D - Directional Distribution	rtion	,
· ·) (0	1	!	9,01	9	!
Traffic Data:		YEAR	ADT	%TRUCK	DHV	CARS	MT	нТ	CARS/2	MT/2	HT/2
							%02	30%			
		2020	4,585	3%	504	489	11	2	245	2	2
		2040	5,135	3%	265	248	12	2	274	9	3

061705

Job Name: Bryant Parkway - Hwy. 183 to Shobe Rd.	Hwy. 183 to Shol	be Rd.									
Roadway Reference: Sho	Shobe Rd. West (Future)	ture)									
County: Saline											
Design Year:	2040										
Year(s) To Be Modeled:	2020 2040										
				Y-Coordinates	ıates						
Roadway Cross-Sections:	2020					_	Note:	DHV = (ADT)(K))(K)		
) = \AHQQ	DDHV = (ADT)(K)(D)		
	2040	Proposed						11%			
								K - Percen	K - Percent of ADT occuring in design hour	curing in	lesign hour
Operating Speed:		30						D - Directio	D - Directional Distribution	tion	
Traffic Data:		YEAR	ADT	%TRUCK	DHV	CARS	MT	H	CARS/2	MT/2	HT/2
							%02	30%			
		2020	4,585	3%	504	489	11	2	245	2	2
		2040	5,135	3%	265	541	12	12	271	9	9

NOISE DATA WORKSHEET

Job No: 061705	-				_						
Job Name: Bryant Parkway - Hwy. 183 to Shobe Rd.	y. 183 to Shobe R	.pg									
Roadway Reference: Bryant F	Bryant Parkway Proejct 1 North of Shobe RdNo-Action	1 North of	Shobe RdNo-,	Action							
County: Saline	П										
Design Year: 2040											
Year(s) To Be Modeled: 2020	2040										
				Y-Coordinates	nates						
Roadway Cross-Sections:	2020						Note:	DHV = (A	DHV = (ADT)(K)		
) = \HQQ	ADT)(K)(D)		
	2040 Pro	Proposed						11%	10 Y O	2 2 2 2 3	
Operating Speed:		35						A - Percen D - Directi	n - Percent of AD I occurin D - Directional Distribution	curing in c ution	N - Percent of AD Loccuring in design nour D - Directional Distribution
Traffic Data:	≻	YEAR	ADT	%TRUCK	ΛHQ	CARS	MT	HT	CARS/2	MT/2	HT/2
							%02	30%			
	2	2020	5,120	3%	263	546	12	2	273	9	3
	2	2040	5,144	3%	999	549	12	2	275	9	3
									N N N	TNM 2.5 VALUES	LUES
									PROF	PROPOSED	
								2040	CARS	%021W	H L30%
								%02	384	8	4
								30%	165	4	2

al PW	- riwy. 163 to olite	DDe Nu.									
Roadway Reference: SI	Shobe Rd. East - No-Action	o-Action									
Sounty: Saline											
Design Year:	2040										
/ear(s) To Be Modeled:	2020 2040										
				Y-Coordinates	ates						
Roadway Cross-Sections:	2020					_	Note:	DHV = (ADT)(K))(K)		
								$) = \Lambda H G G$	DDHV = (ADT)(K)(D)		
	2040	Proposed						11%			
								K - Percent	K - Percent of ADT occuring in design hour	curing in c	design hour
Operating Speed:		30	0					D - Directio	D - Directional Distribution	tion	
raffic Data:		YEAR	ADT	%TRUCK	DHV	CARS	Ψ	Ħ	CARS/2	MT/2	HT/2
							%02	30%			
		2020	3,706	3%	408	396	6	4	198	4	2
		2040	4,549	3%	200	485	11	2	243	2	2

061705

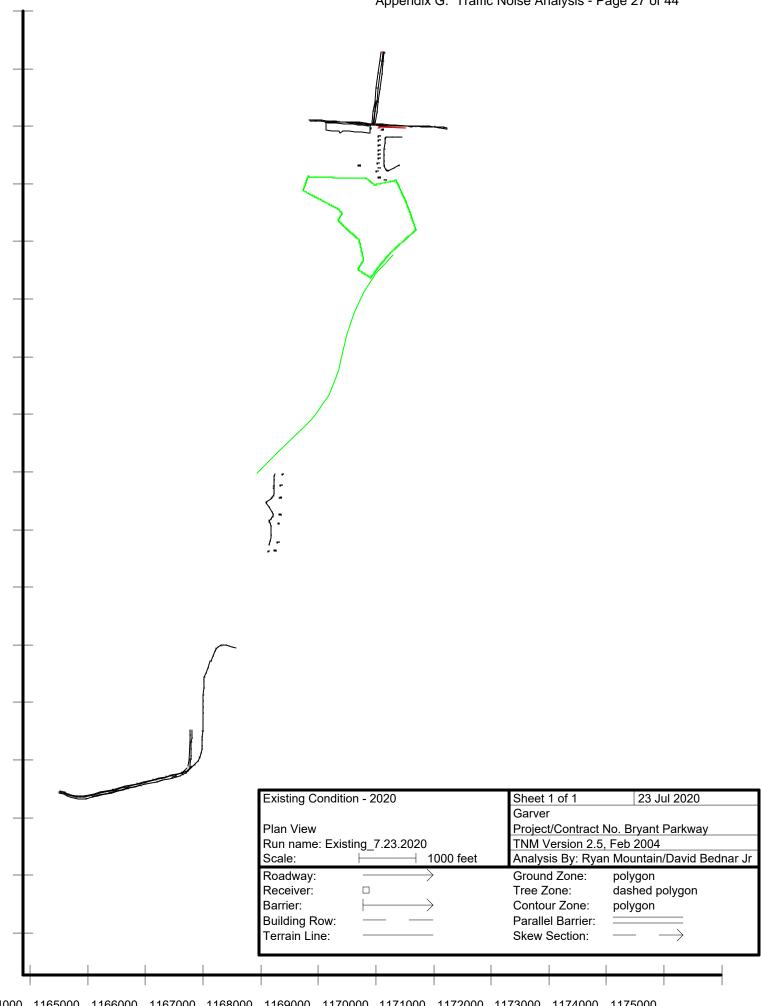
Job Name: Bryant Parkway - Hwy. 183 to Shobe Rd.	/ - Hwy. 183 to Shok	oe Rd.									
Roadway Reference:	Shobe Rd. West - No-Action	o-Action									
County: Saline											
Design Year:	2040										
Year(s) To Be Modeled:	2020 2040										
				Y-Coordinates	nates						
Roadway Cross-Sections:	2020					_	Note:	DHV = (AI	DHV = (ADT)(K)		
) = \HQQ	ADT)(K)(D)		
	2040	Proposed						11%			
								K - Percen	K - Percent of ADT occuring in design hour	curing in c	lesign hour
Operating Speed:		30						D - Direction	D - Directional Distribution	ıtion	
Traffic Data:		YEAR	ADT	%TRUCK	DHV	CARS	MT	H	CARS/2	MT/2	HT/2
							%02	30%			
		2020	4,701	3%	517	501	11	2	251	2	2
		2040	5,267	3%	280	563	12	2	281	9	3

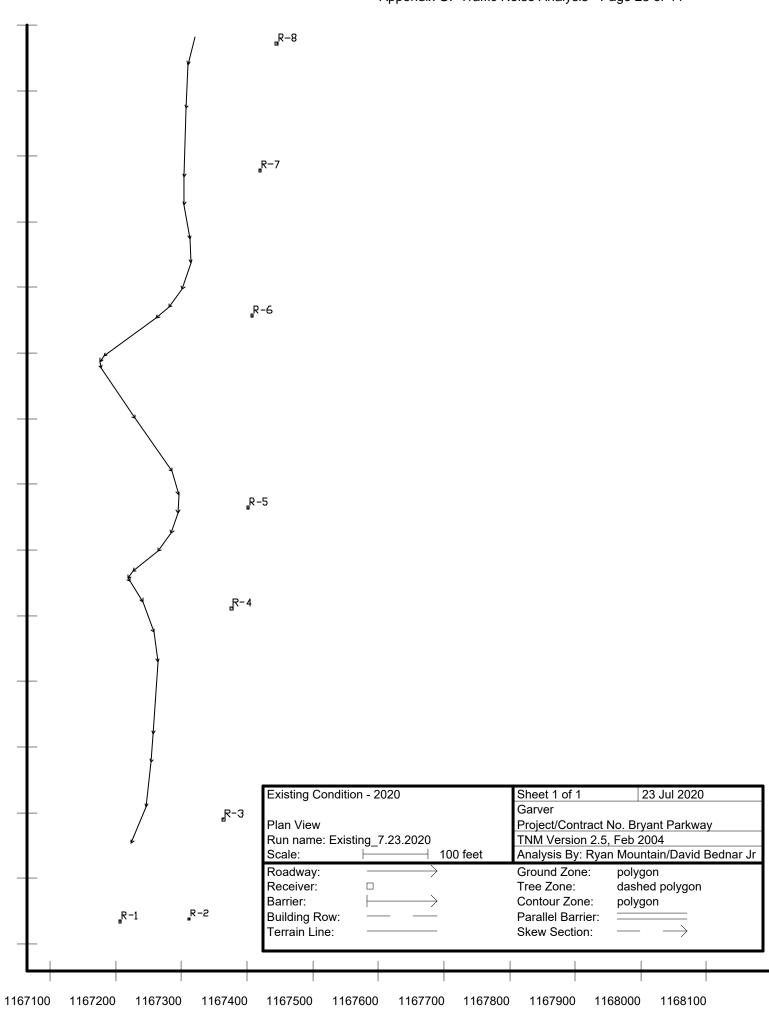


APPENDIX C

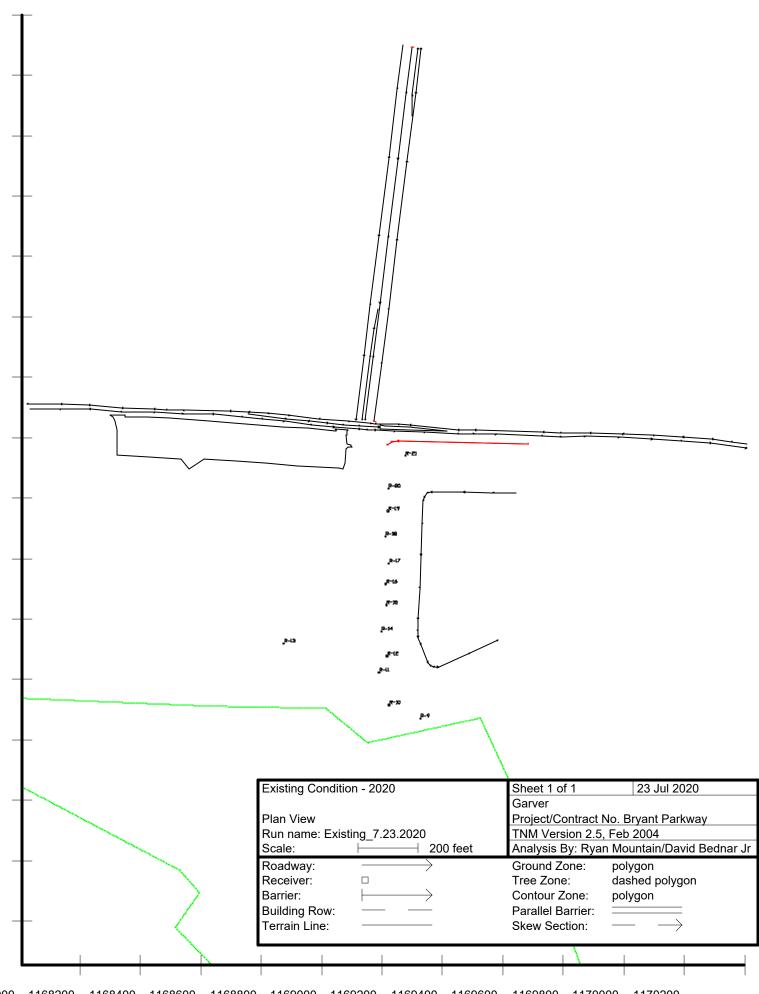
TNM Output Files

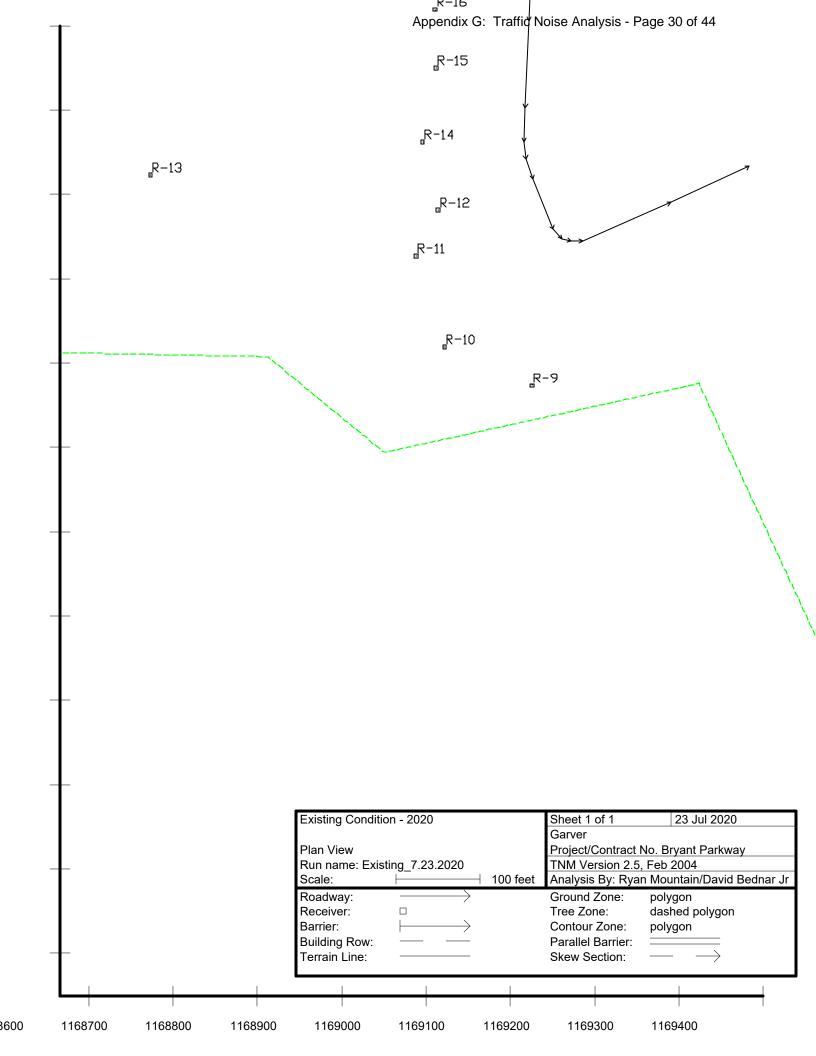


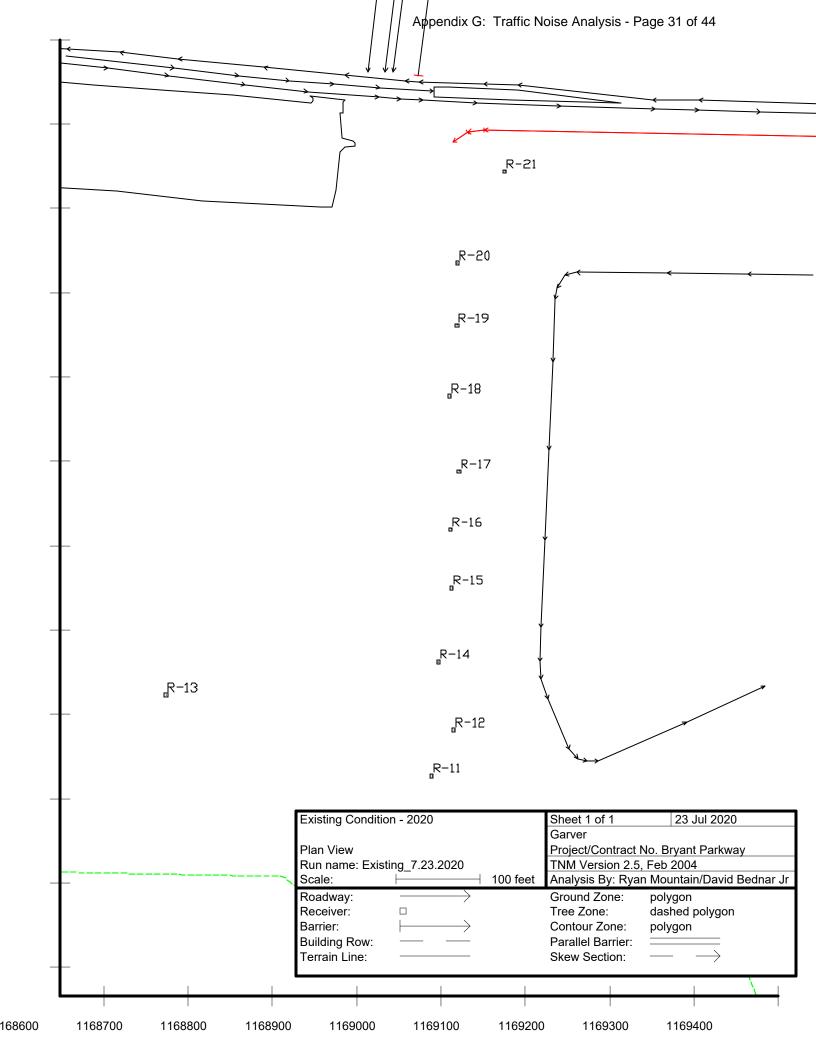




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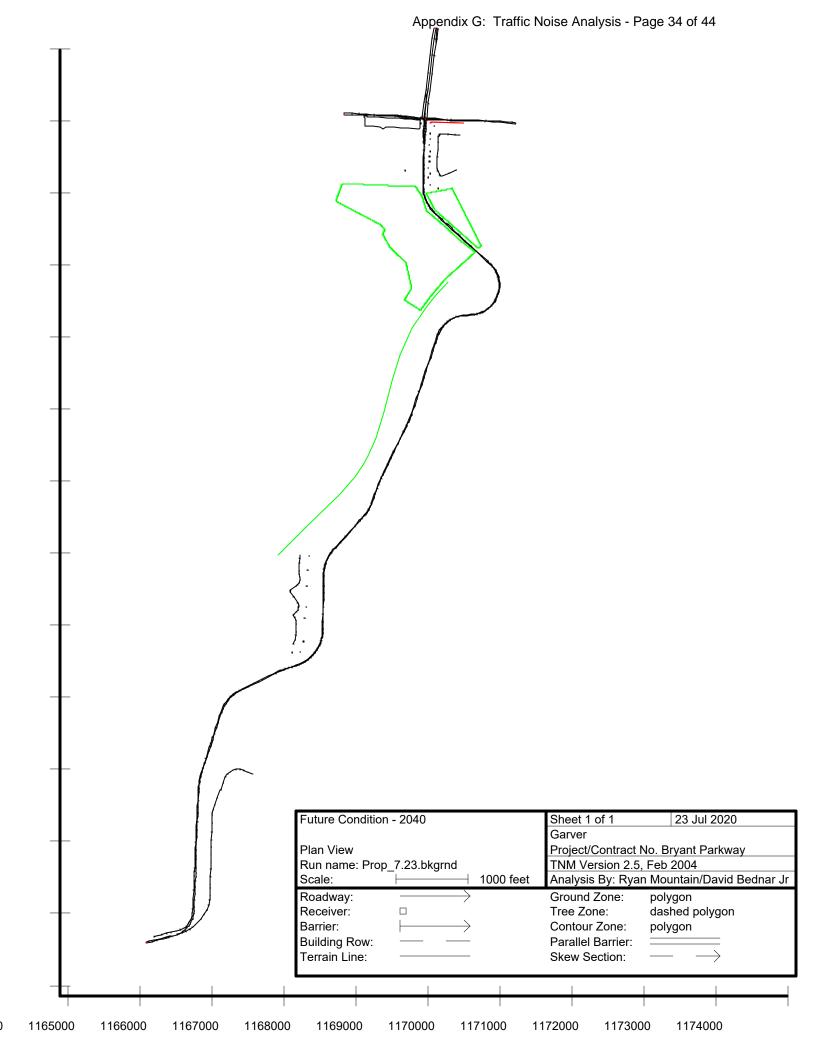
Garver							24 July 2020	020					
Ryan Mountain/David Bednar Jr							TNM 2.5						
							Calculat	Calculated with TNM 2.5	M 2.5				
RESULTS: SOUND LEVELS			-										
PROJECT/CONTRACT:		Bryant	Bryant Parkway Existing Condition	/ ion - 2020									
BARRIER DESIGN:		INPUT	INPUT HEIGHTS					Average	Average pavement type shall be used unless	e shall be us	ed unless		
								a State I	a State highway agency substantiates the use	:y substantia	tes the use	ø	
ATMOSPHERICS:		68 deg	68 deg F, 50% RH	ZH.				of a diffe	of a different type with approval of FHWA	approval of	FHWA.		
Receiver													
Name	Š.	#DNs	Existing	3 No Barrier					With Barrier	L			
			LAeq1h	LAeq1h		Increase	Increase over existing	Type	Calculated	Noise Reduction	ction		
				Calculated	Crit'n	Calculated	d Crit'n	Impact	LAeq1h	Calculated	Goal	Calculated	ated
							Sub'l Inc					minus	
												Goal	
			dBA	dBA	dBA	dB	dB		dBA	dB	dB	dB	
R-1	2	2		0.0		99	19.6	10	19.0	0.0	C	8	-8.0
R-2	4	_		0.0		99	19.7	10	19.7	7 0.0	0	8	-8.0
R-3	∞	2		0.0		99	19.9	10	19.9	0.0	0	8	-8.0
R-4	13			0.0		99	20.4	10	20.4	4 0.0	0	8	-8.0
R-5	16			0.0 20.6		99	20.6	10	20.6	0.0	0	80	-8.0
R-6	17			0.0		99	21.0	10	21.0	0.0	0	8	-8.0
R-7	18	3		0.0		99	21.4	10	21.4	4 0.0	0	8	-8.0
R-8	21	3		0.0		99	21.4	10	21.4		0	8	-8.0
R-9	36	_		0.0		99	38.5	10	38.5	5 0.0	0	8	-8.0
R-10	42	_		0.0		99	39.3	10	39.3	3 0.0	0	8	-8.0
R-11	44	1		0.0		, 99	40.7	10	40.7	0.0	0	8	-8.0
R-12	46	_		0.0 41.0		, 99	1.0 1	10	41.0	0.0	0	8	-8.0
R-13	47	_		0.0		, 99	42.9	10	42.9	0.0	0	8	-8.0
R-14	20	_		0.0 42.3		, 99	42.3	10	42.3	3 0.0	0	8	-8.0
R-15	51	_		0.0		99	43.3	10	43.3	3 0.0	0	8	-8.0
R-16	53	_		0.0 44.3		, 99	14.3	10	44.3	3 0.0	0	8	-8.0
R-17	55	_		0.0		, 99	15.5	10	45.5	5 0.0	0	8	-8.0
R-18	22	_		0.0		, 99	1 47.7	10	47.7	7 0.0	0	8	-8.0
R-19	29	_		0.0		, 99	19.8	10	49.8	8 0.0	0	8	-8.0
R-20	09	1		0.0		99	52.7	10	52.7	0.0	0	8	-8.0
R-21	29	1		0.0		99	53.8	10	53.8	.8 0.0	0	8	-8.0
Dwelling Units		# DNs	Noise Red	Reduction									
			Min	Avg	Max								

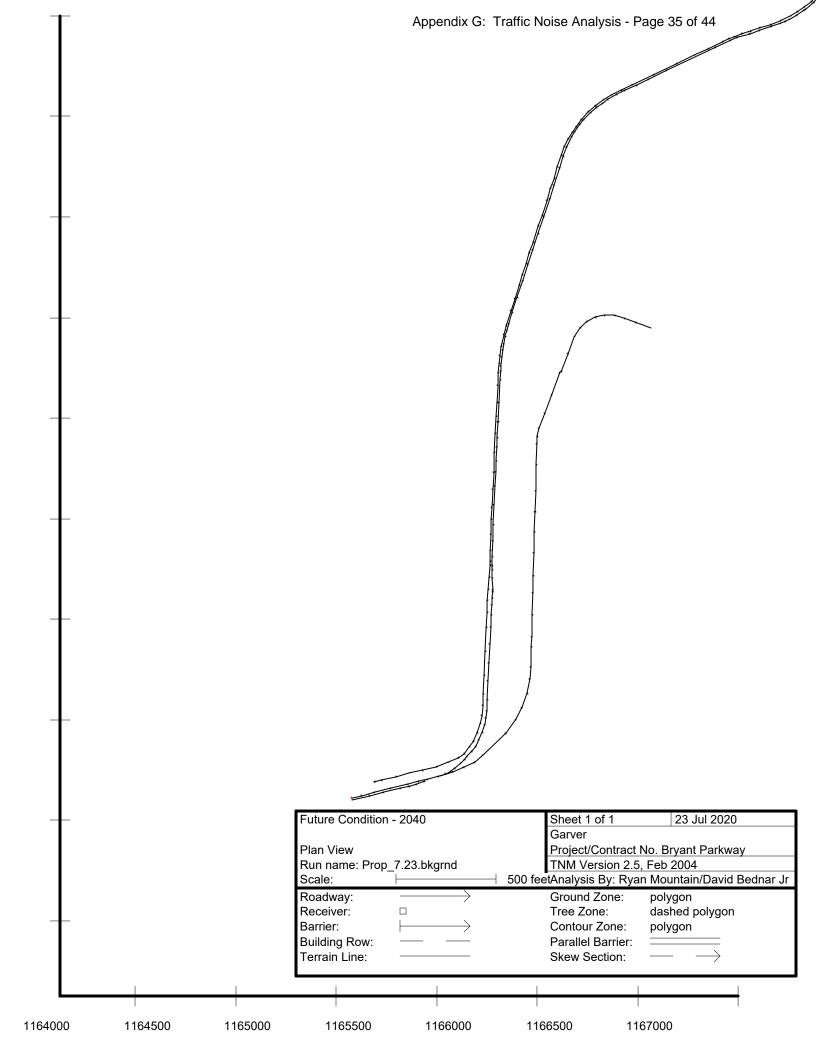
Bryant Parkway

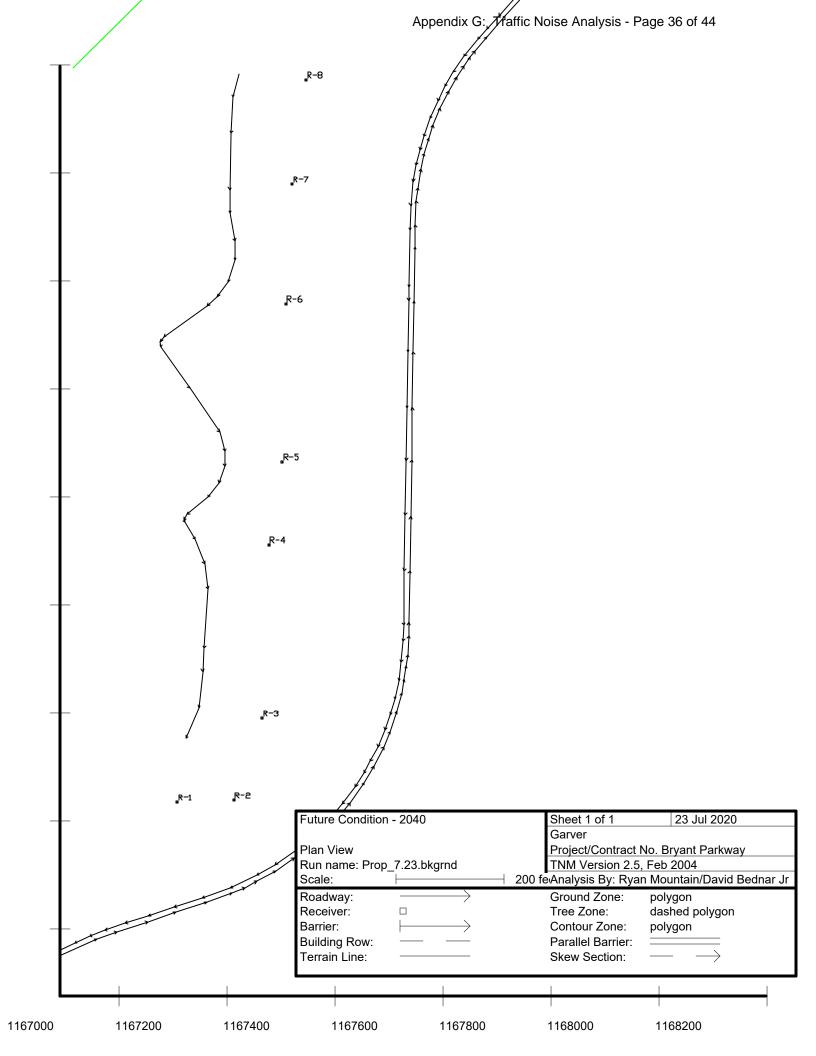
RESULTS: SOUND LEVELS

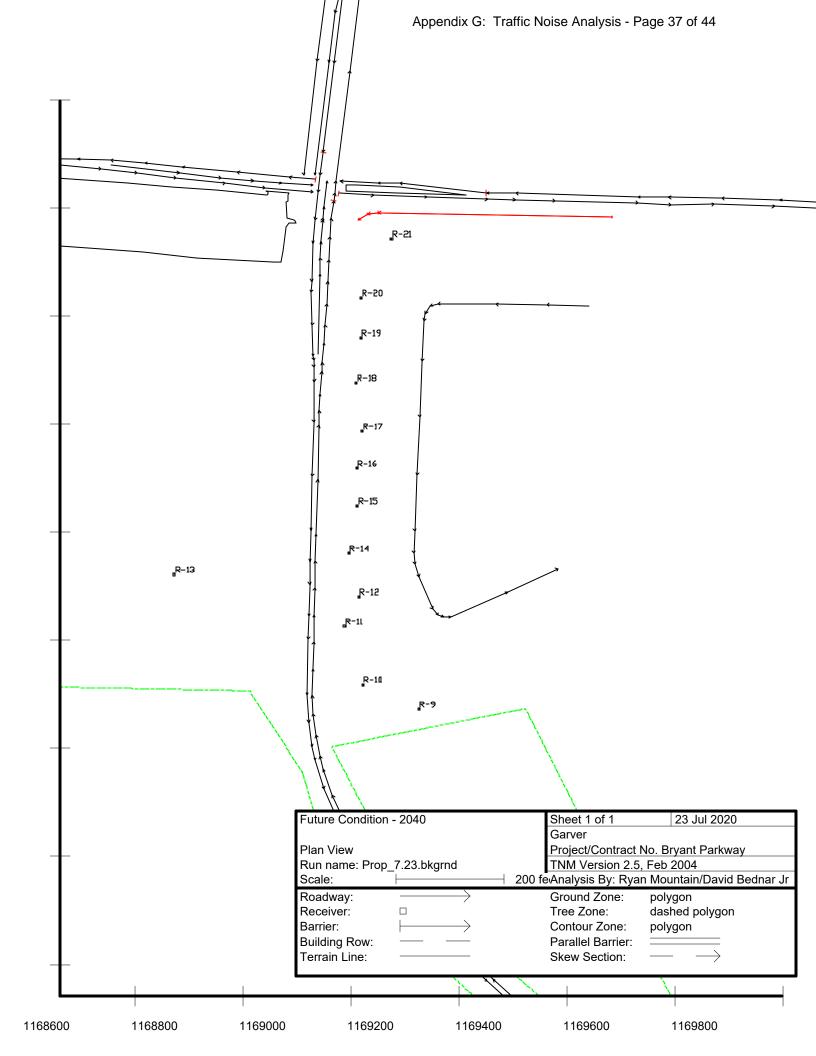
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RESULTS: SOUND LEVELS				Bryant Parkway
	дВ	ф	дB	
All Selected	32 0.0	0.0	0.0	
All Impacted	0.0	0.0	0.0	
All that meet NR Goal	0.0	0.0	0.0	









Garver							24 Ju	24 July 2020						
Ryan Mountain/David Bednar Jr							TNM 2.5	2.5						
							Calcu	lated w	Calculated with TNM 2.5	2.5				
RESULTS: SOUND LEVELS														
PROJECT/CONTRACT:	Δ	ryant		;										
RUN:	ī.	uture (- 2040										
BARRIER DESIGN:	=	NPUT	INPUT HEIGHTS					Á	rerage pa	vement type	Average pavement type shall be used unless	sed unless		
								a	State higl	way agenc	a State highway agency substantiates the use	tes the us	Ф	
ATMOSPHERICS:	Φ	5 deg	85 deg F, 59% RH					ō	a differe	nt type with	of a different type with approval of FHWA	FHWA.		
Receiver														
Name	No.	#DUs	Existing	No Barrier						With Barrier				
			LAeq1h	LAeq1h		Increase	Increase over existing		Type	Calculated	Noise Reduction	ıction		
				Calculated	Crit'n	Calculated	i Crit'n		Impact	LAeq1h	Calculated	Goal	Calculated	ted
							Sub'l Inc	nc Inc					minus	
													Goal	
			dBA	dBA	dBA	фВ	ВВ			dBA	dВ	фВ	ф	
R-1	2	2	44.4	50.0		99	5.6	10	1	50.0	0.0	0:	8	-8.0
R-2	4	-	44.4	52.1		99	7.7	10	1	52.1		0.0	8	-8.0
R-3	80	2	44.4	47.4		99	3.0	10		47.4		0.0	8	-8.0
R-4	13	2	44.4	47.0		99	2.6	9	1	47.0		0.0	8	-8.0
R-5	16	3	44.4	48.2		99	3.8	10	1	48.2		0.0	80	-8.0
R-6	17	3	44.4	48.9		99	4.5	10		48.9		0.0	8	-8.0
R-7	18	3	44.4	48.8		99	4.4	10		48.8		0.0	8	-8.0
R-8	21	3	44.4	47.1		99	2.7	10	1	47.1		0.0	8	-8.0
R-9	36	_	51.5	50.8		99	-0.7	10	1	50.8		0.0	8	-8.0
R-10	42	1	51.6	57.1		99	5.5	10	1	57.1	0.0	0:	8	-8.0
R-11	4	1	51.7	60.3		99	9.8	10	1	60.3	0.0	0:	8	-8.0
R-12	46	1	51.7			99	9.9	10		58.3		0.0	8	-8.0
R-13	47	1	51.9	50.1		99	-1.8	10		50.1		0.0	8	-8.0
R-14	20	1	51.8			99	8.2	10		0.09		0.0	8	-8.0
R-15	51	1	51.9	0.65		99	7.1	10	-	29.0		0.0	8	-8.0
R-16	23	1	52.1	59.2		99	7.1	10	1	59.2		0.0	8	-8.0
R-17	22	1	50.4	58.3		99	7.9	10		58.3		0.0	8	-8.0
R-18	25	_	51.2	58.4		99	7.2	10	1	58.4		0.0	8	-8.0
R-19	26	1	52.3	57.6		99	5.3	10	1	57.6		0.0	8	-8.0
R-20	09	1	54.2	58.9		99	4.7	10		58.9		0.0	8	-8.0
R-21	29	1	55.0	58.5		99	3.5	10		58.5		0.0	8	-8.0
Dwelling Units	#	# DNs	Noise Red	duction										
			Min	Avg	Мах									
				,										

Bryant Parkway

RESULTS: SOUND LEVELS

C:\1-AR\Bryant Pkwy\TNM\Prop_7.23.bkgrnd

7.23.bkgrnd	,
Pkwy\TNM\Prop	
::\1-AR\Bryant	

RESULTS: SOUND LEVELS				Bryant Parkway
	ВВ	dB	ф	
All Selected	32 0.0	0.0	0.0	
All Impacted	0.0	0.0	0.0	
All that meet NR Goal	0.0	0.0	0.0	

Garver							24 July 2020	20					
Ryan Mountain/David Bednar Jr							TNM 2.5						
							Calculated with TNM 2.5	with TNI	M 2.5				
RESULTS: SOUND LEVELS		2											
RUN:		No-Act	Bryain Farkway No-Action Alternative	<u>.</u> .									
BARRIER DESIGN:		INPUT	INPUT HEIGHTS					Average	Average pavement type shall be used unless	e shall be use	ed unless		
								a State hi	a State highway agency substantiates the use	y substantiat	es the use		
ATMOSPHERICS:		68 deg	68 deg F, 50% RH					of a diffe	of a different type with approval of FHWA	approval of h	HWA.		
Receiver													
Name	No.	#DNs	Existing No	No Barrier					With Barrier				
			LAeq1h LA	LAeq1h		Increase over existing		Type	Calculated	Noise Reduction	ction		
			Ca	Calculated	Crit'n	Calculated	Crit'n	Impact	LAeq1h	Calculated	Goal	Calculated	ted
							Sub'l Inc					minus	
												Goal	
			dBA dBA	A	dBA	dB	dB		dBA	dВ	dВ	dB	
R-1	2	2	19.6	19.9	99	5 0.3	3 10	1	19.9	0.0		8	-8.0
R-2	4		19.7	20.1	99	9.0	10	ļ	20.1	0.0		8	-8.0
R-3	8		19.9	20.3	99	5 0.4	10		20.3	3 0.0		8	-8.0
R-4	13	2	20.4	20.8	99	3 0.4	10	1	20.8	3 0.0		8	9.0
R-5	16		3 20.6	21.0	99	9.0	10	1	21.0	0.0		8	-8.0
R-6	17	3		21.4	66		10		21.4			8	-8.0
R-7	18		3 21.4	21.8		5 0.4	10		21.8			8	-8.0
R-8	21	3		21.8			10		21.8			8	-8.0
R-9	36		1 38.5	39.1	99	9.0	3 10	İ	39.1	0.0		8	-8.0
R-10	42	_	39.3	39.8	99	3 0.5	5 10	1	39.8	3 0.0		8	-8.0
R-11	4	_		41.2			5 10	!	41.2			8	-8.0
R-12	46	1	1 41.0	41.5	99	5 0.5	5 10	-	41.5	5 0.0		8	-8.0
R-13	47	7	1 42.9	43.4			5 10	İ	43.4			8	-8.0
R-14	50	1	1 42.3	42.8	99		5 10		42.8	3 0.0		8	-8.0
R-15	51		1 43.3	43.7	99	3 0.4	10	-	43.7	0.0		8	-8.0
R-16	53		1 44.4	44.7	99		3 10	1	44.7	0.0		8	-8.0
R-17	55		1 45.5	45.9	99	3 0.4	10	ļ	45.9	0.0		8	-8.0
R-18	22		1 47.7	48.1	99	3 0.4	10	İ	48.1	0.0		8	-8.0
R-19	29		1 49.8	50.2	99	3 0.4	10	İ	50.2	0.0		8	-8.0
R-20	09	1	1 52.7	53.0	99		3 10		53.0	0.0		8	-8.0
R-21	29	_	1 53.8	54.2	99	5 0.4	10	İ	54.2	0.0		8	-8.0
Dwelling Units		# DNs	Noise Red	nction									
			Min Avg	g/	Мах								

Bryant Parkway

RESULTS: SOUND LEVELS

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RESULIS. SOUND LEVELS					Diyalit Farkway
	дB	σ	В	ф	
All Selected	32	0.0	0.0	0.0	
All Impacted	0	0.0	0.0	0.0	
All that meet NR Goal	0	0.0	0.0	0.0	



APPENDIX D

Alternatives Comparison



Appendix D — Alternatives Traffic Noise Levels Comparison, dB(A) Leq(h)												
	Existing Condition*	Ambient/ Background	Α	lternative E	3	Alternative D**			No-Action			
Modeled Receiver	Existing Level	. •	Existing Level*	Future Level	Change (+/-)	Existing Level*	Future Level	Change (+/-)	Existing Level*	Future Level	Change (+/-)	Noise Impact?
R-1	19.6	44.4	44.4	50	5.6				19.6	19.9	0.3	N
R-2	19.7	44.4	44.4	52.1	7.7				19.7	20.1	0.4	N
R-3	19.9	44.4	44.4	47.4	3	These receivers are signficantly 19.9 20.3 0.4						N
R-4	20.4	44.4	44.4	47	2.6	far away (over 0.25 n	nile) from	20.4	20.8	0.4	N
R-5	20.6	44.4	44.4	48.2	3.8	Alternat	ive D and w	ere not	20.6	21	0.4	N
R-6	21	44.4	44.4	48.9	4.5		evaluated.		21	21.4	0.4	N
R-7	21.4	44.4	44.4	48.8	4.4				21.4	21.8	0.4	N
R-8	21.4	44.4	44.4	47.1	2.7				21.4	21.8	0.4	N
R-9	38.5	51.3	51.5	50.8	-0.7	51.5	50.8	-0.7	38.5	39.1	0.6	N
R-10	39.3	51.3	51.6	57.1	5.5	51.6	57.1	5.5	39.3	39.8	0.5	N
R-11	40.7	51.3	51.7	60.3	8.6	51.7	60.3	8.6	40.7	41.2	0.5	N
R-12	41	51.3	51.7	58.3	6.6	51.7	58.3	6.6	41	41.5	0.5	N
R-13	42.9	51.3	51.9	50.1	-1.8	51.9	50.1	-1.8	42.9	43.4	0.5	N
R-14	42.3	51.3	51.8	60	8.2	51.8	60	8.2	42.3	42.8	0.5	N
R-15	43.3	51.3	51.9	59	7.1	51.9	59	7.1	43.3	43.7	0.4	N
R-16	44.4	51.3	52.1	59.2	7.1	52.1	59.2	7.1	44.4	44.7	0.3	N
R-17	45.5	48.7	50.4	58.3	7.9	50.4	58.3	7.9	45.5	45.9	0.4	N
R-18	47.7	48.7	51.2	58.4	7.2	51.2	58.4	7.2	47.7	48.1	0.4	N
R-19	49.8	48.7	52.3	57.6	5.3	52.3	57.6	5.3	49.8	50.2	0.4	N
R-20	52.7	48.7	54.2	58.9	4.7	54.2	58.9	4.7	52.7	53	0.3	N
R-21	53.8	48.7	55	58.5	3.5	55	58.5	3.5	53.8	54.2	0.4	N

^{*}Decibel addition was used to incorporate background (ambient) noise into the model as noted below: R-1 through R-8 used 44.4 dB; R-9 through R-16 used 51.3 dB; R-17 through R-21 used 48.7 dB. **Alternative D would have the same impacts as Alternative B due to the partial shared alignment.

